

EXPOSURE METHOD

This application claims a benefit of a foreign
priority based on Japanese Patent Application No. 2002-
5 272626, filed on September 19, 2002, which is hereby
incorporated by reference herein in its entirety as if
fully set forth herein.

BACKGROUND OF THE INVENTION

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The present invention relates generally to
exposure, and more particularly to an exposure method
used to fabricate various devices including
semiconductor chips such as ICs and LSIs, display
15 devices such as liquid crystal panels, sensing devices
such as magnetic heads, and image pick-up devices such
as CCDs, as well as fine contact hole patterns used for
micromechanics. Here, the "micromechanics" is
technology for applying the semiconductor IC
20 fabricating technique for fabrications of a fine
structure, thereby creating an enhanced mechanical
system that may operate at a level of micron.

Reduction projection exposure apparatuses have
been conventionally employed which use a projection
25 optical system for projecting a circuit pattern formed
on a mask (reticle) onto a wafer, etc. and for
transferring the circuit pattern, in manufacturing such

fine semiconductor devices as semiconductor memories and logic circuits in the photolithography technology.

The critical dimension transferable by the projection exposure apparatus or resolution is proportionate to a wavelength of light used for exposure, and inversely proportionate to the numerical aperture ("NA") of the projection optical system. The shorter the wavelength is, the better the resolution is. Smaller resolution has recently been demanded with a demand for finer semiconductor devices. Only the exposure light with a small wavelength has the limit to meet this requirement, and the projection optical system is expected to improve resolution using higher NA. At present, a projection optical system has accelerated an improvement of its NA; for example, a projection optical system having $NA = 0.9$ has been developed.

It has been reported that influence on imaging performance becomes non-negligible for high NA due to polarization, because the imaging performance becomes different according to polarizations as an incident angle becomes larger. For high NA, the conventional scalar theory cannot predict the imaging performance in a polarization direction of light. Instead, the vector diffraction theory, which precisely regards light as electromagnetic waves, may describe influence on imaging performance due to polarization.

The imaging performance for two-beam interference is more affected by polarization than that for three-beam interference that forms an image when a 0-th order light and $\pm 1^{\text{st}}$ order diffracted beams interfere with each other.

The three-beam interference forms an image through interference among 0th-order light and $\pm 1^{\text{st}}$ order diffracted beams, while an angle is equal to or less than 45° between 0th-order light and one of $\pm 1^{\text{st}}$ order diffracted beams. On the other hand, an angle is close to 90° at most between 0th-order light and one of $\pm 1^{\text{st}}$ order diffracted beams in the two-beam interference.

It is known that mutually orthogonally polarized wave fronts neither interfere with each other nor form an image. Therefore, even when an angle between $\pm 1^{\text{st}}$ order diffracted beams becomes so close to 90° that they hardly interfere with each other, the influence is small because 0-th order light and one of $\pm 1^{\text{st}}$ order diffracted beams interfere with each other. On the contrary, the impact is serious for the two-beam interference when an angle between 0-th order light and one of $\pm 1^{\text{st}}$ order diffracted beams becomes so close to 90° that they hardly interfere with each other.

As discussed, high NA of the projection optical system is necessary for finer patterns, while it is suggested that the imaging performance deteriorates due to polarization of the high NA and the desired pattern

cannot be formed. In other words, while high NA of the projection optical system is vital to form fine patterns, an associative phenomenon of deteriorated imaging performance needs to be solved. Nevertheless, 5 few reports have discussed polarization-caused influence on the imaging performance in detail, and an exposure apparatus that may control polarization has not yet been proposed.

10 **BRIEF SUMMARY OF THE INVENTION**

Accordingly, it is an exemplified object of the present invention to provide an exposure apparatus which prevents deteriorated imaging performance due to 15 influence of polarization and may form a desired pattern.

An exposure method of one aspect according to the present invention includes the steps of illuminating a pattern formed on a mask using an illumination system 20 that forms an effective light source having a first part that includes only s-polarized light and a second part that mixes s-polarized light and p-polarized light, and projecting, through a projection optical system, light from the mask onto an object to be exposed. The 25 phrase "mixes s-polarized light and p-polarized light" means the light may be linear polarized light, circular

polarized light, non-polarized light different from s-polarized light.

The first part may have an annular shape in which the s-polarized light polarizes in a tangential
5 direction of the annular shape. The second part may have a circular or annular shape that is located inside the first part. Light intensity of the second part may be smaller than that of the first part.

An exposure method of another aspect according to
10 the present invention that uses an illumination system that forms a predetermined effective light source using light from a light source to illuminate a mask, and projects a pattern formed on the mask onto an object to be exposed via a projection optical system includes the
15 steps of splitting the light into s-polarized light and p-polarized light, and forming a first frequency component among frequency components of the effective light source by inputting the s-polarized light into a surface approximately conjugate with a pupil of the
20 projection optical system, and forming a second frequency component lower than the first frequency component by inputting a mixture of the s-polarized light and p-polarized light into the surface. The forming step may be conducted at a side closer to the
25 light source than an optical integrator provided between the light source and the mask.

An exposure method of still another aspect according to the present invention that exposes a pattern formed on a mask onto an object via a projection optical system using light from a light source includes the steps of splitting the light into s-polarized light and p-polarized light, and inputting the s-polarized light into a predetermined area of a pupil in the projection optical system, and inputting light that mixes the s-polarized light and the p-polarized light inside the predetermined area of the pupil.

An exposure method of still another aspect according to the present invention that exposes a pattern formed on a mask onto an object via a projection optical system using light from a light source includes the steps of splitting the light into s-polarized light and p-polarized light, and introducing the s-polarized light into a first part around a center axis that passes through a center of a pupil, in a periphery around the pupil of the projection optical system, and a mixture of the s-polarized light and the p-polarized light into a second part other than the first part in the periphery around the pupil, the first part being parallel to a periodic direction of the pattern. The introducing step may introduce the s-polarized light into a third part around the center axis and an axis orthogonal to the

center axis in the periphery around the pupil of the projection optical system, and a mixture of the s-polarized light and the p-polarized light into a fourth part other than the third part. The polarization
5 direction may be controlled so that the desired pattern is resolved by s-polarization light and the auxiliary pattern is prevented from resolving by the light that mixes the s-polarization light and the p-polarization light.

10 Regarding light from the mask, the above exposure method defines an effective light source distribution on a pupil in a projection optical system with respect to 0-th order diffracted light of light for illuminating the mask.

15 An exposure method of another aspect according to the present invention that uses plural types of light to project onto an object to be exposed through a projection optical system, a mask that arranges a desired pattern of an auxiliary pattern smaller than
20 the desired pattern so that the desired pattern is resolved and the auxiliary pattern is prevented from resolving includes the step of forming a predetermined effective light source by controlling a polarization direction.

25 An illumination system of one aspect according to the present invention includes a mechanism that forms an effective light source by inputting s-polarized

light into a frequency component for resolving a fine pattern, and by inputting light that mixes the s-polarization light and p-polarization light into a frequency component that resolves a pattern other than
5 the fine pattern.

An illumination system of another aspect according to the present invention includes an effective light source that includes a first part that includes only s-polarized light, and a second part that mixes the s-
10 polarized light and p-polarized light.

An exposure apparatus of another aspect according to the present invention includes an exposure mode that may execute the above exposure method.

An exposure apparatus includes the above
15 illumination optical system, and a projection optical system that uses the effective light source formed by said illumination optical system to project a pattern formed on a reticle or mask onto an object to be exposed.

20 A device fabricating method of still another aspect of the present invention includes the steps of exposing an object using the above exposure apparatus, and performing a predetermined process for the exposed object. Claims for a device fabricating method that
25 performs operations similar to that of the above exposure apparatus cover devices as intermediate and final products. Such devices include semiconductor

chips like an LSI and VLSI, CCDs, LCDs, magnetic sensors, thin film magnetic heads, and the like.

Other objects and further features of the present invention will become readily apparent from the following description of the preferred embodiments with
5 reference to accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

10 FIG. 1 is a schematic view showing an exemplary effective light source shape proposed by the present invention.

FIG. 2 is a schematic plane view showing a contact hole pattern.

15 FIG. 3 is a schematic plane view of a desired pattern into which an auxiliary pattern has been inserted to resolve the desired contact hole pattern.

FIG. 4 is a schematic view showing an exemplary effective light source shape to resolve the mask
20 pattern shown in FIG. 3.

FIG. 5 is a plane view that divides the effective light source shape shown in FIG. 4 into two. FIG. 5A is a plane view that typically shows part that contributes resolution of a desired pattern. FIG. 5B
25 is a plane view that typically shows part that restrains an auxiliary pattern from resolving.

FIG. 6A is a plane view showing polarization directions of part that contribute to resolution of a desired pattern, and FIG. 6B is a plane view that typically shows polarization directions of part that
5 restrains an auxiliary pattern from resolving.

FIG. 7 is a plane view that typically shows the effective light source shape shown in FIG. 4 which has controlled polarization directions.

FIG. 8 is a plane view that typically shows the
10 effective light source shape as a variation of the effective light source shape shown in FIG. 7.

FIG. 9 is a plane view that typically shows an effective light source shape as a variation of the effective light source shape shown in FIG. 8.

15 FIG. 10 is a schematic plane view of a mask pattern that arranges holes to form a contact hole pattern.

FIG. 11 is a view that shows a simulation result of an aerial image in one embodiment.

20 FIG. 12 is a typical view for defining s-polarized light and p-polarized light.

FIG. 13 is a typical view of a mask pattern that repeats in an X-axis direction.

FIG. 14 is a graph showing a relationship between
25 a critical dimension and contrast in an L/S pattern.

FIG. 15 is a typical view showing a relationship between a pattern forming direction and a polarization direction.

FIG. 16 is a schematic structure of an exposure
5 apparatus.

FIG. 17 is a typical view showing a relationship between a pattern repeating direction and a polarization direction.

FIG. 18 is a schematic view showing one example of
10 an effective light source shape used to resolve a pattern shown in FIG. 17.

FIG. 19 is a schematic view of one example of an effective light source shape used to resolve a pattern in various directions.

FIG. 20 is a flowchart for explaining how to
15 fabricate devices (such as semiconductor chips such as ICs and LCDs, CCDs, and the like).

FIG. 21 is a detail flowchart of a wafer process as Step 4 shown in FIG. 20.

FIG. 22 is a schematic view showing positions of
20 diffracted beams on a pupil surface for small σ illumination to a binary mask shown in FIG. 3, and moving positions of diffracted beams for oblique incidence illumination.

FIG. 23 is a view showing a relationship between
25 0th order and 1st order beams for oblique incidence illumination to a certain fine pitch pattern.

FIG. 24 is a view that combines four streamlined effective light-source areas (or 0th order beam areas) as partial overlap of two circles.

FIG. 25 is a view of simulated resolution pattern
5 on an object to be exposed.

FIG. 26 is a view showing exposure dose in modified illumination and an image on the object to be exposed corresponding to the exposure dose.

FIG. 27 is a typical view for explaining an
10 effective light source shape.

FIG. 28 is a typical view for explaining an effective light source shape.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

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Referring now to the accompanying drawings, a description will be now given of an exposure apparatus 1 according to the present invention. The same element in each figure is designated by the same reference
20 numeral, and a duplicate description will be omitted.

As a result of earnest research of influence on imaging performance of polarization under high NA, e.g., NA = 0.9 (at the maximum incident angle of 64°), the instant inventors have found that the vector theory
25 states that there is a contrast difference due to polarization states and this difference appears remarkably in the two-beam interference. A description

will now be given of influence of the polarization on the imaging performance when a PSM is used.

The polarization is defined as follows: S-polarized light is polarized light L in a direction perpendicular to a section of a projection optical system OP as shown in FIG. 12A. P-polarized light is polarized light L in a direction parallel to a section of a projection optical system OP as shown in FIG. 12A. Here, FIG. 12 is a typical view that defines p-polarized light and p-polarized light. In other words, s-polarized light polarizes in a Y-axis direction, while p-polarized light polarizes in an X-axis direction, where a Z axis is a progress direction of the light L, the X axis is a direction orthogonal to the Z axis and parallel to a section (or paper surface) of the projection optical system OP, and the Y axis is a direction orthogonal to the section (or paper surface) of the projection optical system OP. The contrast of a pattern 141 will be calculated using the s-polarized light and p-polarized light, which repeats in the X-axis direction as shown in FIG. 13. FIG. 13 is a typical view of a mask pattern that repeats in the X-axis direction.

When an exposure apparatus that has KrF excimer laser with a wavelength λ of 248 nm as a light source, and NA = 0.9 exposes a PSM with p-polarized light, s-polarized light, and non-polarized light, a contrast of

an aerial image is as shown in FIG. 14. The PSM has a line and space ("L/S") pattern that inverts phases of adjacent patterns. Here, FIG. 14 is a graph showing a relationship between a critical dimension and a contrast in an L/S pattern, where an abscissa axis is a critical dimension of the L/S or a half pitch length, and an ordinate axis is a contrast at a best focus or a contrast peak in a focus range.

Referring to FIG. 14, the contrast of the s-polarized light is approximately equal to the contrast of the conventional scalar theory, and the contrast of the p-polarized light drastically reduces to zero when $L/S = 90$ nm. When $L/S = 90$ nm, two diffracted beam directions are orthogonally intersect and these two diffracted beams do not interfere with each other. While the non-polarized state that mixes the s-polarized light and the p-polarized light averages their respective values, the contrast becomes much lower than that expected in the conventional scalar theory.

In order to achieve high-resolution imaging performance as predicted by the scalar theory, the p-polarized light is removed from light that includes the p-polarized light and the s-polarized light, and only the s-polarized light may be used for imaging a pattern. That is, as shown in FIG. 15, s-polarized light that has a polarization direction in the Y-axis

direction is usable to image, at high resolution, a
line pattern 161 as a mask pattern that elongates in a
Y-axis direction. FIG. 15 is a typical view showing a
relationship between a pattern forming direction and a
5 polarization direction.

Referring to the projection optical system OP
shown in FIG. 12, when the light emitted from an exit
pupil EE and directing to a resist surface PR as an
image surface is the s-polarized light, a pattern on an
10 image surface images with high contrast.

Therefore, it is conceivable to insert a pupil
filter into the pupil EE that absorbs or reflects only
the p-polarized light or an optical element that
absorbs or reflects only the p-polarized light between
15 the reticle MS and the pupil EE.

However, when the p-polarized light absorber is
inserted into the pupil EE, this element generates heat
when absorbing light, causing changes of refraction
indexes and shapes to peripheral optical elements, and
20 disadvantageously generating aberration.

When a reflector for reflecting only the p-
polarized light is inserted into the pupil EE, the
reflected light is absorbed in other part of the
projection optical system OP, such as an optical
25 element, similarly causing thermal aberration, or the
light that is not absorbed in other part in the
projection optical system OP scatters in the projection

optical system OP, becomes flare light that does not contribute imaging, and deteriorates contrast.

A similar problem occurs even when an optical element for absorbing or reflecting the p-polarized light is inserted between the reticle MS and the pupil EE, and control over polarization is difficult in the projection optical system OP.

Therefore, it is preferable to control polarization prior to the reticle MS or in the illumination optical system so that only the s-polarized light is irradiated into the reticle MS. Therefore, the reticle MS is irradiated only by the s-polarized light using the illumination optical system shown in FIG. 16. In FIG. 16, it is most effective to control the polarization between an optical system 171 and an optical integrator 172, because an optical system 173 subsequent to the optical integrator 172, particularly in the illumination optical system 170, is to form light suitable for the irradiation to the reticle MS. As a result of an insertion of a filter prior to the optical integrator 172, the optical system 173 subsequent to the optical integrator 172 may correct light scattering and thermal aberration near the filter to some extent. Here, FIG. 16 is a schematic structure of the exposure apparatus.

Imaging performance improves for a binary mask that has a pattern 181 that periodically repeats in an

X-axis direction as shown in FIG. 17, when light 182 that polarizes in a direction orthogonal to a repetitive period is used for illumination. An effective light source in this case, or a distribution projected on a pupil in the projection optical system of an illumination light distribution is preferably a dipole type effective light source shape shown in FIG. 18 which includes bipolar circular effective light sources 191 that have controlled polarization directions 192 in arrow directions in FIG. 18. Here, FIG. 17 is a typical view showing a relationship between a pattern repeating direction and a polarization direction. FIG. 18 is a schematic view showing one example of an effective light source shape used to resolve a pattern shown in FIG. 17.

An effective light source shape 200 is known as shown in FIG. 19 in order to resolve patterns in various directions. The effective light source shape 200 controls a polarization direction in an annular illumination, and more particularly, an effective light source 201 has an annular shape, and the polarization direction of this effective light source 201 is controlled to be a tangential direction (or an arrow direction in FIG. 19) of the annular effective light source 201. Here, FIG. 19 is a schematic view of one example of an effective light source shape used to resolve a pattern in various directions.

In the effective light source shape 200, the more outwardly a position in the effective light source 201 is located, the more light that contributes to resolution of a fine L/S pattern is available.

5 Therefore, a fine periodic pattern resolves when an inside σ_{in} of the effective light source 201 is close to an outside σ_{out} of the effective light source 201. However, the resolution performance of the entire pattern deteriorates, and imaging performance
10 deteriorates in a direction orthogonal to a periodic direction of the L / S pattern and a difference occurs between a critical dimension of a periodic pattern and a periodic pattern of an isolated pattern. In order to avoid this phenomenon, a width of the annular
15 illumination is made large, or the inside σ_{in} of the effective light source 201 is made small.

When a frequency component of an effective light source is considered, it is clear from a graph shown in FIG. 14 that the degree of deterioration of imaging
20 performance by the p-polarized light changes between a high-frequency component around the pupil in the projection optical system and a low-frequency component of the inside. The shorter the half pitch length as an abscissa axis is in the graph shown in FIG. 14, the
25 larger the light incident angle becomes; thus, the deterioration of imaging performance by the p-polarized light becomes large as an angle between two beams

becomes close to a right angle. The deterioration of imaging performance by the p-polarized light becomes small when the half pitch length becomes long.

Therefore, the low frequency component inside the pupil of the projection optical system is less subject to contrast deterioration of an image due to differences of polarization directions, and the polarization direction does not have to be considered. On the contrary, in the low-frequency component inside the pupil of the projection optical system, the light that has no specific polarization direction or mixes the s-polarized light and p-polarized light improves resolution performance in view of homogeneity, etc. so as to entirely resolve the non-fine pattern, a non-periodic pattern or a non-L/S and comparatively large pattern. Therefore, light of a wide range of frequency components is needed from the inside of the pupil to the outside in order to improve the entire image quality of various patterns formed on a reticle.

However, the imaging performance depends upon a polarization direction of light of a high-frequency component outside the pupil, but does not depend upon a polarization direction of light of a low-frequency component outside the pupil. Here, the light that mixes the s-polarized light and p-polarized light may be linearly polarized, circularly polarized light or non-polarized light different from the s-polarized

light. In addition, the linear polarization may be polarized in a direction from a center of a pupil of the projection optical system to the outside, or a radial direction.

5 For the above reasons, the present invention proposes effective light source shapes 10A and 10B as shown in FIGs. 1A and 1B, so as to improve resolution performance of a fine pattern and homogeneity of resolution performance of an L/S pattern and an
10 isolated pattern.

 The effective light source shape 10A shown in FIG. 1A uses s-polarized light that polarizes in a tangential direction of an annular shape for a first, annular part 12A from σ_{in} to σ_{out} in the effective
15 light source 16A in order to resolve a fine pattern, and a non-polarized state that mixes the s-polarized light and p-polarized light for a second, circular part 14A inside σ_{in} in order to entirely resolve a non-fine pattern.

20 When the light intensity of the second part 14A inside σ_{in} is made smaller than that of the first part 12A outside σ_{in} , the resolution may be maintained for a fine pattern. Equation 1 below defines σ_{in} where L is a length of a fine pattern for which resolution
25 performance is demanded to improve, λ is a wavelength, and NA is a numerical aperture of a projection optical system: $\sigma_{in} = \lambda / (4L \cdot NA)$

Alternatively, the effective light source shape 10B shown in FIG. 1B may achieve the same effect. The effective light source shape 10B uses s-polarized light that polarizes in a tangential direction of an annular shape for a first, annular part 12B from σ_{in1} to σ_{out} in the effective light source 16B in order to resolve a fine pattern, and a non-polarized state that mixes the s-polarized light and p-polarized light for a second, annular part 14B from σ_{in1} to σ_{in2} in order to entirely resolve a non-fine pattern.

In other words, an effective light source shape at a pupil in the projection optical system makes the s-polarized light incident upon an axis parallel to a pattern period around the effective light source that is likely to rely upon a direction of the pattern period, and distributes the light that mixes s-polarized light and p-polarized light at part that do not depend upon the direction of the pattern period.

When the light intensity of the second part 14B from σ_{in1} to σ_{in2} is made smaller than that of the first part 12B outside σ_{in1} , the resolution for a fine pattern is maintained. The effective light source shape 10B does not deteriorate resolution for a fine pattern by shielding the light of a part 18B as a light shielding part inside σ_{in2} .

Alternatively, an effective light source shape 10C shown in FIG. 1C may be used for a mask that composes

mainly of patterns that extend in an X-axis direction
and/or a Y-axis direction. The effective light source
10C uses s-polarized light that polarizes in abscissa
and ordinate directions of an annular shape for a first,
5 annular part 12C from σ_{in} to σ_{out} in the effective
light source 16C in order to resolve a fine pattern,
and a non-polarized state that mixes the s-polarized
light and p-polarized light for a second, circular part
14C inside σ_{in} in order to entirely resolve a non-fine
10 pattern.

When the mask pattern that composes mainly of
patterns that extend in an X-axis and/or a Y-axis
direction and the effective light source shape 10A
shown in FIG. 1A is used as the effective light source,
15 such polarization directions are undesirably included
as contribute to resolution of patterns in a direction
other than X-axis and Y-axis directions. These
polarization components are not parallel to patterns,
i.e., patterns that extend in an X-axis and/or a Y-axis
20 direction, and the s-polarized light component reduces
by that amount.

Therefore, when a mask pattern consists of
patterns that extend in the X-axis direction and/or Y-
axis direction, an effective light source that consists
25 of polarization components parallel to the patterns,
such as that shown in FIG. 1C, would rather improve

resolution performance of an exposure apparatus and
simplify a structure of an illumination system.

Of course, the resolution suitable for a fine
pattern is maintained similar to the above, when the
5 light intensity of the second part 14C inside σ in is
made smaller than that of the first part 12C outside
 σ in, or when the light is shielded inside σ in. A
further effect may be expected when a mask pattern is
provided with a polarization film that transmits
10 particular polarized light.

A description will be given of another example to
resolve a contact hole pattern. While a mask pattern
101 shown in FIG. 10 is usually used to resolve a
contact hole pattern 21 shown in FIG. 2, it is known
15 that the resolving power improves when a mask pattern
30 is used as shown in FIG. 3 which arranges not only a
desired pattern 31 to form the contact hole pattern 21
but also an auxiliary pattern 32 smaller than the
desired pattern 31. An exposure method for resolving
20 only the desired pattern 31 by illuminating a mask that
includes such patterns with an effective light source
shape 40 (FIG. 40) that includes a crossed light
shielding part 41 and a circular effective light source
42 is referred to as "Exposure Method I". Here, FIG. 2
25 is a schematic plane view of the contact hole pattern
21. FIG. 3 is a schematic plane view of a mask pattern
that inserts the auxiliary pattern 32 into the desired

pattern 31. FIG. 4 is a schematic view showing one example of the effective light source 40 for resolving the mask pattern 30 shown in FIG. 3.

The mask shown in FIG. 3 is characterized in that
5 it sets t / d to be 0.5, preferably 0.7 or greater where "t" is an aperture diameter of the desired pattern 31 to resolve the contact-hole pattern 21 and "d" is an aperture diameter of the unresolved auxiliary pattern 32 to assist the desired pattern 31 in
10 resolving.

A description will now be given of the Exposure Method I in detail.

Only the desired contact hole pattern may be exposed with good resolving power onto an object, such
15 as a wafer, by illuminating this mask 30 using plural types of light, such as crossed oblique incidence illumination (referred to as enhancement illumination part) to resolve the desired contact hole pattern, and illumination (referred to as restraint illumination
20 part) to restrain the crossed oblique incidence illumination from resolving the auxiliary pattern (in other words, to limit the exposure dose for the auxiliary pattern (a little increased exposure dose) and to enhance the exposure dose for the desired
25 contact-hole pattern (much increased exposure dose)).

When the mask 30 that has a small pitch in the contact holes is illuminated with small σ illumination,

diffracted beams deviate from the pupil surface in the projection optical system in the exposure apparatus except for the 0-th order diffracted beam. More specifically, there occur the 0-th order diffracted beam 10 and diffracted beams 11-18 of other orders as shown in FIG. 22A, and diffracted beams except for the 0-th order diffracted beam deviate from the pupil surface, whereby no pattern is formed under this condition. Here, FIG. 22A is a typical view showing positions of diffracted beams on the pupil surface in the projection optical system when the mask 30 is subject to small σ illumination.

Therefore, illumination should allow the diffracted beams 11-18 to enter the pupil. For example, in order to allow illustrative two diffracted beams 10 and 15 to enter the pupil in the projection optical system shown in FIG. 22A, the illumination light may be moved to form oblique incidence illumination as shown in FIG. 22B. This oblique incidence illumination may enable the 0-th order diffracted beam and one of $\pm 1^{\text{st}}$ order diffracted beams 15 to enter both ends in the pupil in the projection optical system, and interference between these two diffracted beams incident upon the pupil forms linear interference bands at a regular pitch on the object.

FIG. 23 shows a relationship between the 0-th order diffracted beam and the 1^{st} order diffracted beams

in oblique incidence illumination for a mask pattern with fine pitches. The 0-th order diffracted beam for area "a" generates $\pm 1^{\text{st}}$ order diffracted beams like "b" and "c". In this figure, a shape of the area "a" allows one of $\pm 1^{\text{st}}$ order diffracted beams to enter the pupil. Left and right circles of the pupil in the projection optical system have the same diameter as the pupil diameter in the projection optical system, and their centers are offset from the center of the pupil by a predetermined amount or an interval between 10 and 15 in FIG. 22. In other words, the oblique incidence illumination that arranges all the 0-th order diffracted beam in the area "a" enables one of $\pm 1^{\text{st}}$ order diffracted beams 15 to enter the pupil, and interference between these two diffracted beams forms linear interference bands at a regular pitch on the object.

Similarly, the oblique incidence illumination that arranges the 0-th order diffracted beam in the area "b" shown in FIG. 23 enables one of $\pm 1^{\text{st}}$ order diffracted beams 15 to enter the pupil in the area "a".

As shown in FIG. 24, four streamlined effective light-source areas as a combination area of two circles would form linear fringe bands on an object to be exposed at a regular pitch in longitudinal and lateral directions, and strong and weak parts appear at two-dimensional pitches at intersection points overlapping

light intensity distributions. In other words, the above enhancement illumination part corresponds to four (beveled) streamlined areas having a longitudinal direction in a direction orthogonal to a radial direction of crossed pupil as shown in FIG. 24. The other part (*i.e.*, part other than beveled part in the pupil in the projection optical system) corresponds to the above restraint illumination part.

The desired contact-hole pattern 31 on the mask 30 is made larger than the auxiliary pattern 32 and thus has stronger light intensity than the peripheral, forming the desired contact hole pattern. However, as shown in FIGs. 25A and 25B, the mere crossed oblique incidence illumination would result in the resolution of the auxiliary pattern, creating an unnecessary pattern other than the desired contact-hole pattern. Here, FIG. 25 is a view of simulated resolved pattern on the object corresponding to the right effective light source shape.

As shown in FIG. 26, the exposure dose of a thin solid ray resolves not only the desired pattern P1 but also auxiliary pattern P2 when sliced at the exposure-dose threshold or resist threshold shown by a thin dotted line in FIG. 26 where the desired contact hole pattern P1 has a desired diameter value. Here, FIG. 26 shows the exposure dose and an image on the object corresponding to the exposure dose for the crossed

oblique incidence illumination and inventive modified illumination.

Accordingly, it is conceivable to add the effective light source distribution, *i.e.*, the above
5 restraint illumination part that allows only one diffracted beam to enter the pupil surface, to the effective light source distribution shown in FIG. 24. Preferably, the diffracted beam is the 0-th order diffracted light as the only one diffracted beam. FIG.
10 27 shows an exemplary effective light source distribution.

The exposure dose shows like a thick solid ray as shown in FIG. 26 when the mask 30 is illuminated using an effective light source distribution shown in FIG. 28
15 that has a crossed blank at its center and is close to an addition between the effective light source distribution shown in FIG. 24 that allows two diffracted beams to enter the pupil and the effective light-source distribution shown in FIG. 27 that enables
20 one diffracted beam to enter the pupil. That is, the exposure dose particularly increases at part corresponding to the desired contact hole pattern 31 on the mask 30, and provides the desired pattern P3 in which the dummy resolution pattern P2 disappears at the
25 exposure dose threshold or resist threshold shown by a thick dotted line in FIG. 26 where the desired contact-hole pattern has a desired diameter value.

In summary, Exposure Method I characteristically uses the effective light source shape 40 shown in FIG. 4, which has two functions understandably. In other words, the effective light source shape 40 may be divided into two, as shown in FIGs. 5A and 5B. Four parts 51 in FIG. 5A serve to effectively resolve the desired pattern 31, but they result in possibly resolving the auxiliary pattern 32 around the desired pattern 31. On the other hand, four parts 52 in FIG. 5B clarify an outline of the desired pattern 31 and serve to restrain the auxiliary pattern 32 from resolving. Therefore, only the desired pattern 31 resolves and the auxiliary pattern 32 does not when the mask 30 shown in FIG. 3 is exposed with the effective light source shape 40 shown in FIG. 4. Here, FIG. 5 is a plane view that dissolves the effective light-source shape 40 shown in FIG. 4 into two, FIG. 5A is a schematic plane view of the part 51 that contribute to resolution of the desired pattern 31, and FIG. 5B is a schematic plane view of the part 52 that restrains the auxiliary pattern 32 from resolving.

The above Exposure Method I may also employ an effective light source that controls polarization directions. More specifically, the effective light source shape 40 forms an effective light source shown in FIG. 6A which uses s-polarized light for four parts 51 for resolving the fine desired pattern 31, and an

effective light source shown in FIG. 6B which uses a non-polarized light that mixes s-polarized light and p-polarized light for the part 52 for emphasizing an outline of the desired pattern 31. Thus, the effective
5 light source shape 40 is suitable for the Exposure Method I, since it combines effective light sources shown in FIGs. 6A and 6B, and its polarization directions are controlled as shown in FIG. 7.

In other words, the effective light source shape
10 on a pupil in the projection optical system makes the s-polarized light incident upon an axis that is parallel to a pattern period around the effective light source and passes through a center of the pupil, and distributes the light that mixes s-polarized light and
15 p-polarized light on other part.

The effective light source 40 shown in FIG. 7 is effective to the usual exposure as well as the Exposure Method I. Here, FIG. 6A is a plane view that typically shows a polarization direction of the part 51 that
20 contributes to resolution of the desired pattern 31, and FIG. 6B is a plane view that typically shows a polarization direction of the part 52 that restrains resolution of the auxiliary pattern 32. FIG. 7 is a plane view that typically shows the effective light
25 source shape 40 whose polarization direction is controlled.

An effective light source shape 40A shown in FIG. 8 may be used as a variation of the effective light source shape 40 shown in FIG. 7. The effective light source shape 40A includes a rectangular light shielding part 41A and a circular effective light source 42A outside the light shielding part 41A. The effective light source shape 40A shown in FIG. 8 is useful for the Exposure Method I when polarized light in longitudinal and lateral directions, *i.e.*, directions parallel to the X-axis and Y-axis directions are controlled to be s-polarized light, and an oblique direction, *i.e.*, a direction that forms 45° relative to the X-axis and Y-axis direction is controlled to be a non-polarized light that mixes s-polarized light and p-polarized light. Here, FIG. 8 is a plane view that typically shows the effective light source shape 40A as a variation of the effective light source shape 40 shown in FIG. 7.

An effective light source shape 40B shown in FIG. 9 is also useful for the Exposure Method I when the effective light source shape 40A directs polarized light outside a circle SC that contains the rectangular light shielding part 41A to a tangential direction of the circle SC, and sets polarized light inside the circle SC to be a non-polarized light that mixes s-polarized light and p-polarized light. While the circle SC in FIG. 9 contacts the light shielding part

41A, its radius may be made larger according to critical dimensions in a pattern, etc. The effective light source shapes 40A and 40B are also useful like the effective light source shape 40, for normal exposures as well as the Exposure Method I. Here, FIG. 9 is a plane view that typically shows the effective light source shape 40B as a variation of the effective light source shape 40A shown in FIG. 8.

A description will now be given of a result of simulation that assumes an exposure apparatus that uses KrF excimer laser having a wavelength of 248 nm as a light source and a NA of its projection optical system of 0.9. The projection exposure apparatus generally provides a reduction projection exposure. In case of reduction projection exposure, the pattern size to be produced is different from a mask pattern by a magnification depending upon the exposure apparatus. The magnification of the exposure apparatus depends upon its machine type, and this application converts the pattern size on the mask into the size on the wafer or an object to be exposed.

For example, for a pattern of 120 nm on the wafer, when the magnification on the projection exposure apparatus is 0.25, a pattern of 480 nm should be actually formed on the mask, and when the magnification on the projection exposure apparatus is 0.20, a pattern of 600 nm should be formed on the mask. However, for

simplicity purposes, the instant application converts the size of the mask pattern into the size on the wafer or object to be exposed, and calls the pattern of 120 nm.

5 EXAMPLE

The target pattern sets pitch in a lateral direction $p = 180$ nm, i.e., a hole diameter to be a contact hole pattern 21 of 90 nm, a hole pitch in a transverse direction to be 90 nm, and a hole pitch in a longitudinal direction as $2p = 360$ nm in FIG. 2. A usual binary mask has a difficulty in exposing such a fine pattern, and the Exposure Method I is used preferably.

The effective light source shape 40 having a crossed light shielding part 41 may be used to expose the mask shown in FIG. 3 that inserts the auxiliary pattern 32 of 70 nm into a period of 180 nm in longitudinal and lateral directions, wherein the effective light source shape 40 shown in FIG. 4 has $\sigma =$ 0.9, $a = 0.7$ and $b = 0.55$.

FIG. 11A shows a resultant two-dimensional aerial image at the time of best focus for simulation that uses the effective light source 40 in a non-polarization state.

On the other hand, FIG. 11B shows a resultant two-dimensional aerial image at the time of best focus for simulation that uses the effective light source 40A

shown in FIG. 7 that provides tangential polarization in longitudinal and lateral directions and a non-polarization in an oblique direction.

Referring to FIGs. 11A and 11B, the effective
5 light source shape 40A that controls polarization results in a sharper aerial image of the desired pattern 31 than that using the effective light source shape 40 in a non-polarization.

It is understood that a non-polarization state
10 shown in FIG. 11A blurs an image and lowers contrast, while FIG. 11B provides a sharp image close to an image obtained in the scalar theory. While the contrast drop as seen in the non-polarization state is a big issue in resolving a fine pattern, it has been discovered that
15 use of the Exposure Method I and effective light source shape 40A that controls polarization may resolve a fine pattern. A periodic pattern is subject to an effect of controlled polarization, and the Exposure Method I although pseudo may relatively easily obtain an effect
20 of illumination that controls polarization so as to form a periodic pattern.

The instant example has been confirmed that an effect of an effective light source that controls polarization in the Exposure Method I, in particular,
25 an effect of the effective light source shape 40A shown in FIG. 7. Similarly, the effects of the effective

light source shapes 40 and 40B shown in FIGs. 8 and 9 are also confirmed.

While a description of the instant example uses $NA = 0.9$, this exposure method is advantageously useful for higher NA and finer patterns. More apparent effect may be seen in immersion exposure using NA equal to or greater than 0.1. Since it is generally reported that influence of polarization for high NA starts when NA is equal to or larger than 0.70, NA smaller than 0.9 also achieve similar effects.

The effective light source shapes that control polarization as shown in FIGs. 1, 7 to 9 are implemented as a shape of an aperture stop 174 arranged just after an exit surface of an optical integrator 172 as a pupil surface in the illumination optical system 170 in an exposure apparatus in FIG. 16. The aperture stop 174 is provided at a position approximately conjugate with a pupil in a projection optical system OP in the exposure apparatus, and an aperture shape of the aperture stop corresponds to an effective light source shape on the pupil surface in the projection optical system. Therefore, the effective light source shape 10B shown in FIG. 1 is implemented as an aperture stop 10B that has the light transmission parts 12B and 14B, and light shielding part 18B. The effective light source shape 40 shown in FIG. 7 is implemented as the aperture stop 40 that has light transmitting part 42

and light shielding part 41. The effective light source shape 40A shown in FIG. 8 is implemented as the aperture stop 40A that has light transmitting part 42A and light shielding part 41A. The effective light source shape 40B shown in FIG. 9 is implemented as the aperture stop 40B that has light transmitting part 42B and light shielding part 41B. An illumination optical system and exposure apparatus having the above aperture stop, or an exposure apparatus having an exposure mode that may execute an exposure method that controls polarization as discussed.

Referring now to FIGs. 20 and 21, a description will be given of an embodiment of a device fabricating method using the above exposure apparatus. FIG. 20 is a flowchart for explaining a fabrication of devices (i.e., semiconductor chips such as IC and LSI, LCDs, CCDs, etc.). Here, a description will be given of a fabrication of a semiconductor chip as an example. Step 1 (circuit design) designs a semiconductor device circuit. Step 2 (mask fabrication) forms a mask having a designed circuit pattern. Step 3 (wafer preparation) manufactures a wafer using materials such as silicon. Step 4 (wafer process), which is referred to as a pretreatment, forms actual circuitry on the wafer through photolithography using the mask and wafer. Step 5 (assembly), which is also referred to as a posttreatment, forms into a semiconductor chip the

wafer formed in Step 4 and includes an assembly step (e.g., dicing, bonding), a packaging step (chip sealing), and the like. Step 6 (inspection) performs various tests for the semiconductor device made in Step 5, such as a validity test and a durability test. Through these steps, a semiconductor device is finished and shipped (Step 7).

FIG. 21 is a detailed flowchart of the wafer process in Step 4. Step 11 (oxidation) oxidizes the wafer's surface. Step 12 (CVD) forms an insulating film on the wafer's surface. Step 13 (electrode formation) forms electrodes on the wafer by vapor disposition and the like. Step 14 (ion implantation) implants ion into the wafer. Step 15 (resist process) applies a photosensitive material onto the wafer. Step 16 (exposure) uses the exposure apparatus to expose a circuit pattern on the mask onto the wafer. Step 17 (development) develops the exposed wafer. Step 18 (etching) etches parts other than a developed resist image. Step 19 (resist stripping) removes disused resist after etching. These steps are repeated, and multilayer circuit patterns are formed on the wafer. The device fabrication method of this embodiment may manufacture higher quality devices than the conventional one. Thus, a device fabrication method using the inventive lithography and resultant devices constitute one aspect of the present invention. While

the object to be processed illustratively uses a silicon wafer, a glass plate, a spherical semiconductor, etc. may be used for the object.

Further, the present invention is not limited to
5 these preferred embodiments, and various variations and modifications may be made without departing from the scope of the present invention.

As discussed, the inventive exposure method may prevent deteriorated imaging performance due to
10 influence of polarization and may form desired patterns.